**Presentation for:** 

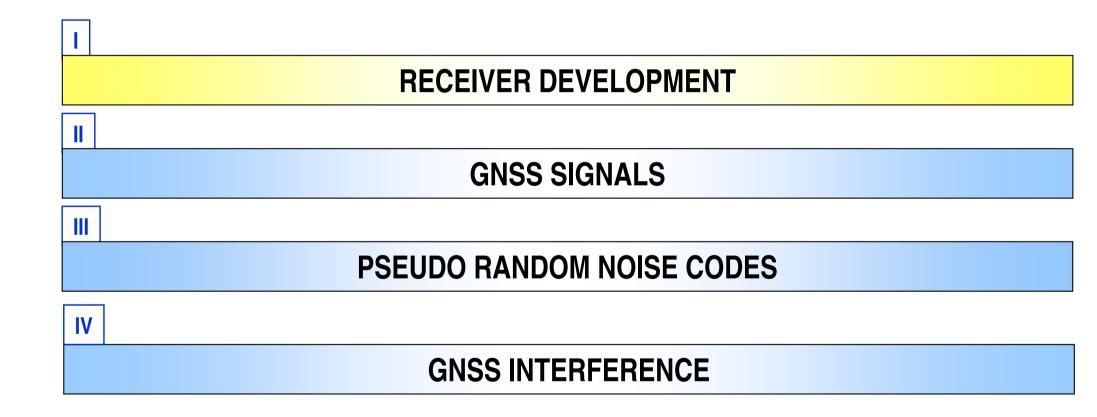
14<sup>th</sup> GNSS Workshop November 01, 2007 Jeju Island, Korea



# RECEIVER DEVELOPMENT, SIGNALS, CODES AND INTERFERENCE

Stefan Wallner, José-Ángel Ávila-Rodríguez, Guenter W. Hein Institute of Geodesy and Navigation, University FAF Munich, Germany

# **CONTENTS**

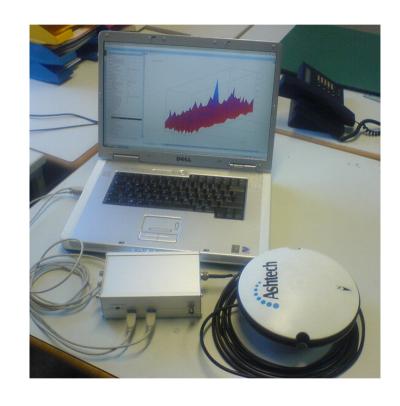




# SOFTWARE GNSS RECEIVER - ipexSR

- ✓ High end, multi-frequency, real-time capable
- Civil signal tracking of all-in-view GPS/Galileo/SBAS satellites
- ✓ Development in C++ classes and modules
- To be run on conventional PC
- ✓ Input IF samples from
  - Triple frequency (L1/E1, L2, L5/E5a) USB Front-End
  - Data files in post-processing mode

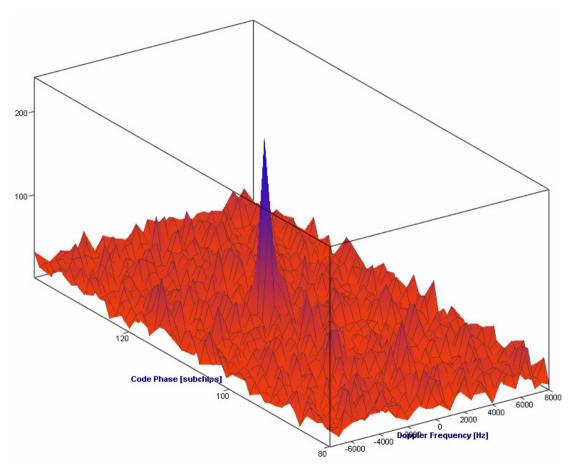
Frequency	Bandwidth	Sample Rate	ADC Res.
L1, E1	15/20 MHz	40.96 MHz	2/4 Bits
L2	15/20 MHz	40.96 MHz	2/4 Bits
L5, E5a	15/20 MHz	40.96 MHz	4 Bits





# **ARCHITECTURE - ACQUISITION**

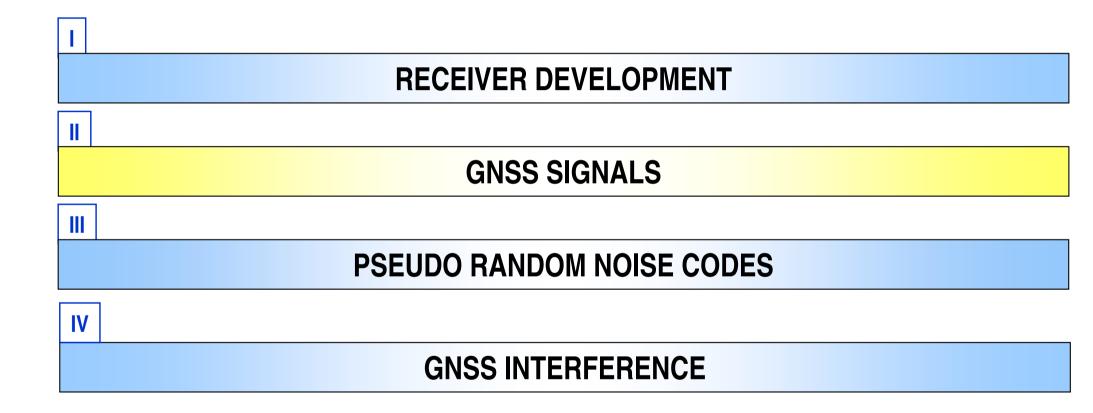
- ✓ Two acquisition procedures depending on available information
  - Acquisition by navigation solution
  - ▼ Two level FFT-based acquisition
- Acquisition of strong signals by conventional coherent integration
- ✓ High sensitivity acquisition
  - →Combination of coherent and non-coherent integration, including parallel interference cancellation



3D Acquisition plot generated by the software receiver when acquiring a GPS satellite.

Institute of Geodesy and Navigation

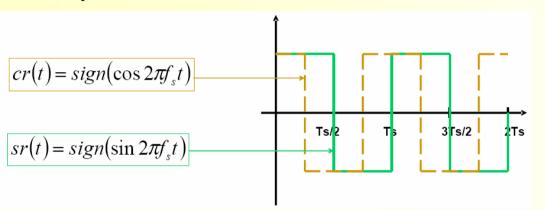
# **CONTENTS**

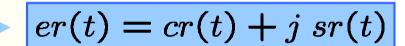




- ✓ Objectives of Alternative BOC (AltBOC) on E5a/b
  - Multiplexing of 2 or 4 navigation signal components each with own PRN code on 2 nearby frequencies
- ✓ Solution 1
  - ✓ Generation of 2 QPSK separately and combine them with OMUX
    - → Band limitation of OMUX removes high frequency component → loss of accuracy
- ✓ Solution 2
  - Combination of signals at base-band, up-conversion to mean frequency
    - → One carrier → phase coherency between two frequencies guaranteed
    - → One amplification chain
    - → Higher bandwidth → higher accuracy
  - Constant envelope modulation has to be assured

### ✓ Complex BOC subcarrier

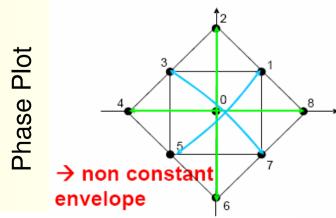




4 component AltBOC

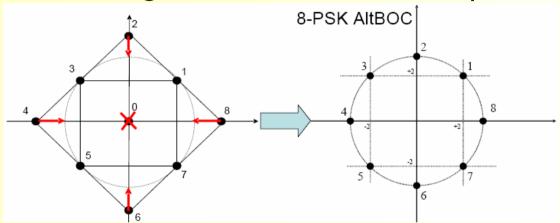
$$x(t) = (c_1(t) + c'_1(t)) er(t) + (c_2(t) + c'_2(t)) er^*(t)$$

	Signal C1		-1	7	-1	-1	۲-	
	Signal C2		-1	-1	-1	-1	1	
	Signal C'1		-1	-1	1	1	۲	
	Signal C'2		-1	1	-1	-1	1	
	t mod Ts	[0, Ts/4[	5	0	4	3	6	
		[Ts/4, Ts/2[	1	8	0	7	0	:
		[Ts/2, 3Ts/4[	1	0	8	7	2	
		[3Ts/4, Ts [	5	4	0	3	0	



Modulation Table

### Achieving the constant envelope



### Constellation points

$$\exp\left(\frac{jk\pi}{4}\right), \ k \in \{1, \dots, 8\}$$

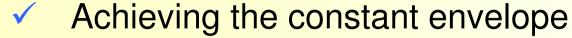
### New signal description

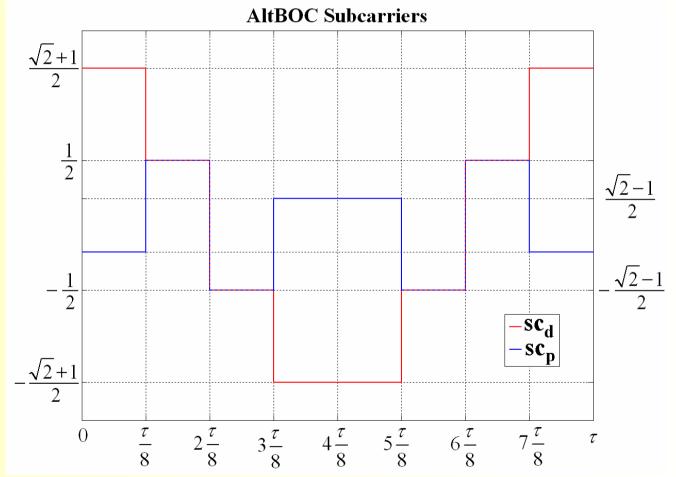
$$x(t) = \frac{1}{2\sqrt{2}} \left[ \frac{\left(c_1(t) + jc_1'(t)\right)er(t) + \left(c_2(t) + jc_2'(t)\right)er^*(t)}{\left(\bar{c}_1(t) + j\bar{c}_1'(t)\right)\bar{e}r(t) + \left(\bar{c}_2(t) + j\bar{c}_2'(t)\right)\bar{e}r^*(t)} \right]$$

$$er(t) = sc_d(t) + j \ sc_d(t - T_s/4)$$

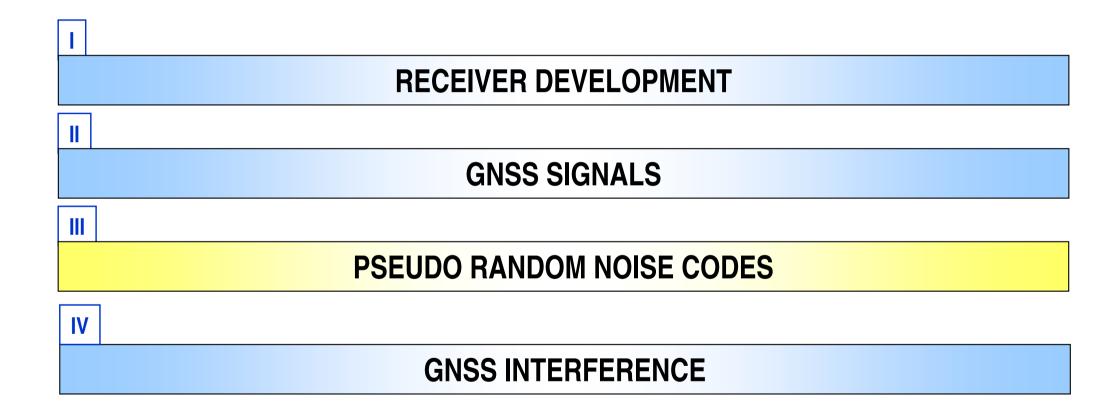
$$e^{\overline{r}(t)} = sc_p(t) + j \ sc_p(t - T_s/4)$$

→ 4-level signal!





# **CONTENTS**





### **PSEUDO RANDOM NOISE CODES**

- Pseudo Random Noise (PRN) codes are essential element in every CDMA based GNSS
- Keystone to distinguish one SV from another
- All currently implemented civilian codes based on Linear Feedback Shift Registers (LFSR)
  - → Identical approach as in 1<sup>st</sup> generation GPS
- Galileo E1 OS and GPS L1C are bringing up new code concepts
  - ✓ (Galileo E1 OS: random codes) ← Focus
  - ✓ GPS L1C: Weil-based codes

### **OPTIMIZATION CRITERIA**

- Optimization for every receiver implementation and application not feasible
  - → Use code centric approach
- Code centric approach based on
  - Auto- and crosscorrelation
    - Concentration on (maximum) or distribution possible
- ✓ Consideration of 
  → GPS a
  - Even and odd correlation (data bit or secondary code bit flip)
  - Doppler frequency offsets

Galileo approach

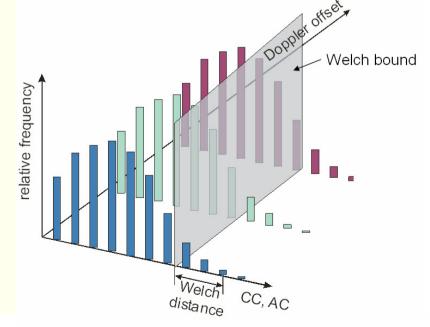
### GALILEO CODE OPTIMIZATION CRITERIA

Correlation values compared against Welch-bound

Welch Bound  $\Phi_{min}$  is the theoretical minimum of correlation that can be obtained for a code length n within a set of M codes:

$$\Phi_{\mathsf{min}} = n \sqrt{\frac{M-1}{Mn-1}}$$

- every correlation value above Welch bound degrades performance
- → Criteria of Welch distance for autoand crosscorrelation considering Doppler dependency applied (slight modifications to achieve acquisition and tracking criteria)

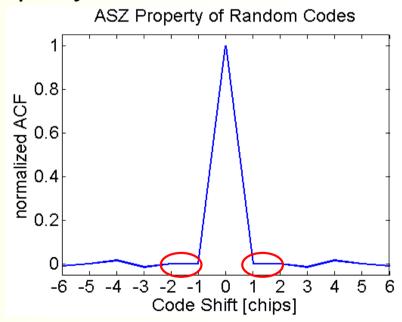


# GALILEO E1 OS / E6 CS CODE OPTIMIZATION

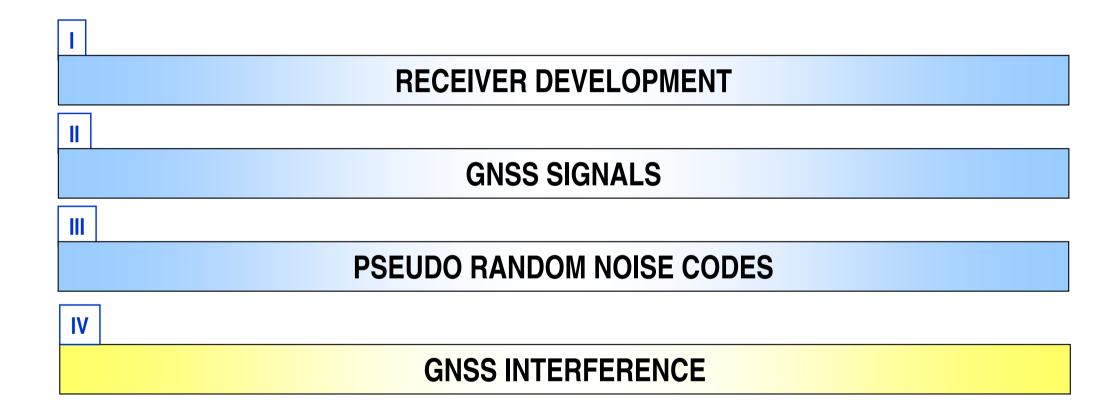
- ✓ Random codes (memory codes) for Galileo E1 OS and E6 CS
- Most flexible code generation and optimization approach
- Codes can be driven to fulfill special properties
  - Autocorrelation Sidelobe Zero (ASZ) property
  - ✓ Ideal or weakened balance

#### However

- Number of choices to set 0's and 1's unimaginably high
  - → Application of genetic algorithms for optimization



# **CONTENTS**





### SOURCES OF INTERFERENCE

- Interference introduced from external sources
  - Radar
  - ✓ DVB-T
  - ✓ DME, TACAN, JTADS
  - Unintentional interference





- Interference within GNSS
- Signal interference
- PRN code interference

Radio frequency compatibility

### SIGNAL INTERFERENCE

- ✓ Intrasystem Interference
  - Within each system
- ✓ Intersystem Interference
  - Interference that a GNSS/RNSS will suffer due to other GNSS/RNSS, augmentation systems to be considered
  - ✓ Intersystem Interference too high
    - correct functioning of current working GNSS receivers could be affected if new GNSS is entering the stage



# INTERFERENCE CRITERION $\Delta(C/N_0)_{eff}$

Degradation of  $C/N_0$  due to intersystem interference

$$\Delta \left(\frac{C}{N_0}\right)_{\rm eff} [{\rm dB}] = 10 \log_{10} \left(1 + \frac{I_{\rm inter}}{N_0 + I_{\rm intra}} + \frac{I_{\rm inter}}{I_{\rm interop}}\right)$$

where:

$$I_{ ext{inter}} = rac{\sum\limits_{i=1}^{M_{ ext{inter}}}\sum\limits_{j=1}^{N_{ ext{inter}}}C_{j}^{i}\kappa_{js}^{i}}{\int_{-rac{eta_{r}}{2}}^{rac{eta_{r}}{2}}G_{s}(f+f_{ ext{dop}_{s}})\,\mathrm{d}f}$$

with Spectral Separation Coefficient (SSC):

$$\kappa_{js}^{i} = \int_{-\frac{\beta_r}{2}}^{\frac{\beta_r}{2}} G_j^i(f + f_{\mathsf{dop}_j}) G_s(f + f_{\mathsf{dop}_s}) \, \mathrm{d}f$$

Rec. power of signal i from SV j

Number of visible SV from non- $N_{\mathsf{inter}}$ 

desired system

 $M_{\mathsf{inter}}$ Number of interfering signals from

non-desired system in scenario

PSD of desired signal

 $G_j^i$ PSD of signal i from SV j

Front-end bandwidth

 $N_0$ Noise floor: -201.5 dBW/Hz

 $f_{\mathsf{dop}_j}$ Doppler frequency for SV j

 $f_{\mathsf{dop}_s}$ Doppler frequency of desired

> signal Institute of Geodesy and Navigation
>
> Institut for Endmessung und Navigation

# INTERFERENCE CRITERION $\Delta(C/N_0)_{eff}$

Degradation of  $C/N_0$  due to intersystem interference

$$\Delta \left(\frac{C}{N_0}\right)_{\rm eff} [{\rm dB}] = 10 \log_{10} \left(1 + \frac{I_{\rm inter}}{N_0 + I_{\rm intra} + I_{\rm interop}}\right)$$

where:

$$I_{ ext{intra}} = rac{\sum\limits_{i=1}^{M_{ ext{intra}}}\sum\limits_{j=1}^{N_{ ext{intra}}}C^i_j\kappa^i_{js}}{\int_{-rac{eta_r}{2}}^{rac{eta_r}{2}}G_s(f+f_{ ext{dop}_s})\,\mathrm{d}f}$$

with Spectral Separation Coefficient (SSC):

$$\kappa_{js}^{i} = \int_{-\frac{\beta_r}{2}}^{\frac{\beta_r}{2}} G_j^i(f + f_{\mathsf{dop}_j}) G_s(f + f_{\mathsf{dop}_s}) \, \mathrm{d}f$$

Rec. power of signal i from SV j

 $N_{\mathsf{intra}}$ Number of visible SV from

desired system

 $M_{\mathsf{intra}}$ Number of desired and interfering

signals from desired system

PSD of desired signal

 $G_j^i$ PSD of signal *i* from SV *j* 

Front-end bandwidth

 $N_0$ Noise floor: -201.5 dBW/Hz

 $f_{\mathsf{dop}_j}$ Doppler frequency for SV j

 $f_{\mathsf{dop}_s}$ Doppler frequency of desired

> signal Institute of Geodesy and Navigation
>
> Institut for Endmessung und Navigation

# INTERFERENCE CRITERION $\Delta(C/N_0)_{eff}$

Degradation of  $C/N_0$  due to intersystem interference

$$\Delta \left(\frac{C}{N_0}\right)_{\rm eff} [{\rm dB}] = 10 \log_{10} \left(1 + \frac{I_{\rm inter}}{N_0 + I_{\rm intra}} + \frac{I_{\rm inter}}{I_{\rm interop}}\right)$$

Where: 
$$M_{ ext{interop}} N_{ ext{interop}} \sum_{i=1}^{N_{ ext{interop}}} \sum_{j=1}^{C_j^i \kappa_{js}^i} C_j^i \kappa_{js}^i$$

$$= \int_{-\frac{\beta_r}{2}}^{\frac{\beta_r}{2}} G_s(f + f_{ ext{dop}_s}) \, \mathrm{d}f$$

with Spectral Separation Coefficient (SSC):

$$\kappa_{js}^{i} = \int_{-\frac{\beta_r}{2}}^{\frac{\beta_r}{2}} G_j^i(f + f_{\mathsf{dop}_j}) G_s(f + f_{\mathsf{dop}_s}) \, \mathrm{d}f$$

Rec. power of signal i from SV j

Ninterop Number of visible SV from nondesired system

 $M_{\text{interop}}$  Number of interoperable signals

from non-desired system

PSD of desired signal

 $G_j^i$ PSD of signal i from SV j

Front-end bandwidth

 $N_0$ Noise floor: -201.5 dBW/Hz

 $f_{\mathsf{dop}_j}$ Doppler frequency for SV j

 $f_{\mathsf{dop}_s}$ Doppler frequency of desired

> Institute of Geodesy and Navigation
>
> Institut für Erdmessung und Navigation signal

# INTERFERENCE CRITERION (C/N<sub>0</sub>)<sub>eff</sub>

 $\checkmark$  Min. effective  $C/N_0$ 

$$\left(\frac{C}{N_0}\right)_{\text{eff}} [\text{dB} - \text{Hz}] = \frac{C}{N_0 + I_{\text{intra}} + I_{\text{inter}} + I_{\text{interop}}}$$

- Degradation of C/N<sub>0</sub> and min. effective C/N<sub>0</sub> are complementary criteria
  - ✓ Degradation of C/N<sub>0</sub> criteria limits impact of every single GNSS/RNSS
  - ✓ Min. effective C/N<sub>0</sub> criteria provides full picture of interference environment

### INTERSYSTEM CROSSCORRELATION

- ✓ GPS L1C and Galileo E1 OS implementing both MBOC(6,1,1/11)
  - → Interoperability
- However: PRN codes could interfere with each other
- Different strategies
  - Pure code correlation
  - Rx (receiver based) code correlation

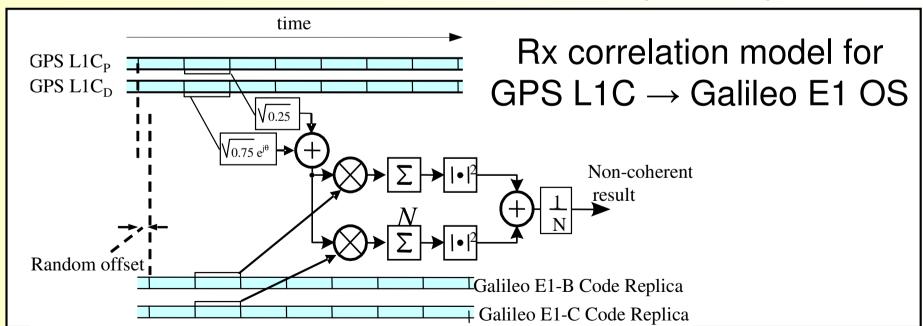


Further strategies to be investigated

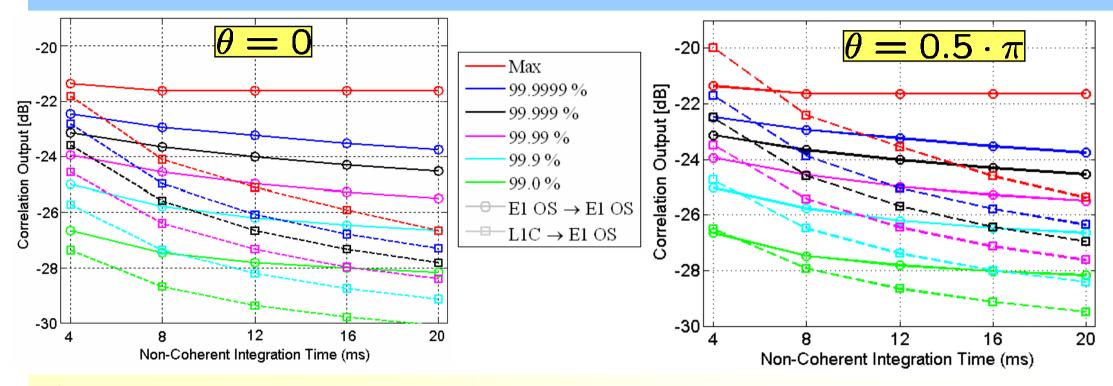


### RX CORRELATION APPROACH

- Receiver centric approach
- Non-coherent integrations
- Pre-correlation time identical to primary code duration
- Consideration of modulation scheme and power split



# **RX CORRELATION ONTO GALILEO E10S**



- For more than 1 non-coherent integration max. and all percentiles of intersystem correlation smaller than intrasystem correlation
- Reason: due to different code length no superposition of correlation values in intersystem case



### **SUMMARY**

### Receiver development

Presentation of ipexSR Software receiver developed at Institute of Geodesy and Navigation, University FAF Munich

### **Signals**

- ✓ AltBOC in E5 is Galileo's signal with largest bandwidth → best performance achievable
- Innovative multiplexing technique

#### **PRN** codes

Random codes and Weil codes completely new code design approaches

#### Interference

Assessment of signal and code interference extremely important with more and more GNSS/RNSS systems transmitting in identical frequency bands



### RECEIVER DEVELOPMENT, SIGNALS, CODES AND INTERFERENCE

# **THANKS FOR YOUR ATTENTION !!**

**Contact:** Stefan Wallner

stefan.wallner@unibw.de

University FAF Munich

Werner-Heisenberg-Weg 39

85577 Neubiberg

Germany



### RECEIVER DEVELOPMENT, SIGNALS, CODES AND INTERFERENCE

### **Reference Documents**

#### **Receiver Development**

Anghileri M. et al., "Performance Evaluation of a Multi-frequency GPS/Galileo/SBAS Software Receiver", Proceedings of ION GNSS 2007, 25-28 September 2007, Fort Worth, Texas, USA

### Signals

✓ Rebeyrol E. et al., "BOC Power Spectrum Densities", Proceedings of ION NTM 2005, 24-26 January 2005, Long Beach, California, USA

#### PRN Codes

- ✓ Wallner S. et al., "Galileo E1 OS and GPS L1C Pseudo Random Noise Codes Requirements, Generation, Optimization and Comparison", Proceedings of ION GNSS 2007, 25-28 September 2007, Fort Worth, Texas, USA
- ✓ **Soualle F. et al.**, "Spreading Code Selection Criteria for the Future GNSS Galileo", Proceedings of GNSS 2005, 19-22 July 2005, Munich, Germany

#### Interference

- ▼ Titus B.M. et al., "Intersystem and Intrasystem Interference Analysis Methodology", Proceedings of ION GPS 2003, 09-12 September 2003, Portland, Oregon, USA
- ✓ Wallner S. et al., "Interference Calculation between GPS and Galileo", Proceedings of ION GNSS 2005, 13-16 September 2005, Long Beach, California, USA